

Z-FORCE

DIY Turbo Jet Engine : Z-GS1

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Main purpose

- Build operating downscale jet engine for model jet aircraft.

NOTE

- we don't show all sketches in this presentation because the project is in progress and some parts must be changed.

Construction of each part

- Running and sliding fits

More Clearance (Close to Top of The Chart)	Clearance Fits	Description	Hole Basis	Shaft Basis
		Free Running	H9/d9	D9/h9
Loose Running		H11/c11	C11/h11	
Easy Running		H8/f8	F8/h8	
Sliding		H7/g6	G7/h6	
Close Clearance		H8/f7	F8/h7	
Locational Clearance		H7/h6	H6/h7	
More Interference (Close to Bottom of The Chart)	Transition Fits	Location- slight interference	H7/k6	K7/h7
	Interference Fits	Location/Transition	H7/n6	N7/h6
		Location/Interference	H7/p6	P7/h6
		Medium Drive Fit	H7/s6	S7/h6
	Force Fit	H7/u6	U7/h6	

ISO shaft Tolerances

Example: Nominal Size 3mm-6mm; $-270\mu\text{m} = -270(10^{-3}) = -0.270\text{mm}$

Grade	NOMINAL SHAFT SIZES (mm)																			
	3	6	10	18	30	40	50	65	80	100	120	140	160	180	200	225	250	280	315	355
Over	3	6	10	18	30	40	50	65	80	100	120	140	160	180	200	225	250	280	315	355
Up to and incl.	6	10	18	30	40	50	65	80	100	120	140	160	180	200	225	250	280	315	355	400
a12	-270 -390	-280 -430	-290 -470	-300 -510	-310 -560	-320 -570	-340 -640	-360 -660	-380 -730	-410 -760	-460 -860	-520 -920	-580 -980	-660 -1120	-740 -1200	-820 -1280	-920 -1440	-1050 -1570	-1200 -1770	-1350 -1920
d6	-30 -38	-40 -49	-50 -61	-65 -78	-80 -96		-100 -119		-120 -142		-145 -170			-170 -199			-190 -222			-210 -246
e6	-20 -28	-25 -34	-32 -43	-40 -53	-50 -66		-60 -79		-72 -94		-85 -110			-100 -129			-110 -142			-125 -161
e13	-20 -200	-25 -245	-32 -302	-40 -370	-50 -440		-60 -520		-72 -612		-85 -715			-100 -820			-110 -920			-125 -1015
f5	-10 -15	-13 -19	-16 -24	-20 -29	-25 -36		-30 -43		-36 -51		-43 -61			-50 -70			-56 -79			-62 -87
f6	-10 -18	-13 -22	-16 -27	-20 -33	-25 -41		-30 -49		-36 -58		-43 -68			-50 -79			-56 -88			-62 -98
f7	-10 -22	-13 -28	-16 -34	-20 -41	-25 -50		-30 -60		-36 -71		-43 -83			-50 -96			-56 -108			-62 -119
g5	-4 -9	-5 -11	-6 -14	-7 -16	-9 -20		-10 -23		-12 -27		-14 -32			-15 -35			-17 -40			-18 -43
g6	-4 -12	-5 -14	-6 -17	-7 -20	-9 -25		-10 -29		-12 -34		-14 -39			-15 -44			-17 -49			-18 -54
g7	-4 -16	-5 -20	-6 -24	-7 -28	-9 -34		-10 -40		-12 -47		-14 -54			-15 -61			-17 -69			-18 -75
h4	0 -4	0 -4	0 -5	0 -6	0 -7		0 -8		0 -10		0 -12			0 -14			0 -16			0 -18
h5	0 -5	0 -6	0 -8	0 -9	0 -11		0 -13		0 -15		0 -18			0 -20			0 -23			0 -25
h6	0 -8	0 -9	0 -11	0 -13	0 -16		0 -19		0 -22		0 -25			0 -29			0 -32			0 -36
h7	0 -12	0 -15	0 -18	0 -21	0 -25		0 -30		0 -35		0 -40			0 -46			0 -52			0 -57
h8	0 -18	0 -22	0 -27	0 -33	0 -39		0 -46		0 -54		0 -63			0 -72			0 -81			0 -89
h9	0 -30	0 -36	0 -43	0 -52	0 -62		0 -74		0 -87		0 -100			0 -115			0 -130			0 -140
h10	0 -48	0 -58	0 -70	0 -84	0 -100		0 -120		0 -140		0 -160			0 -185			0 -210			0 -230

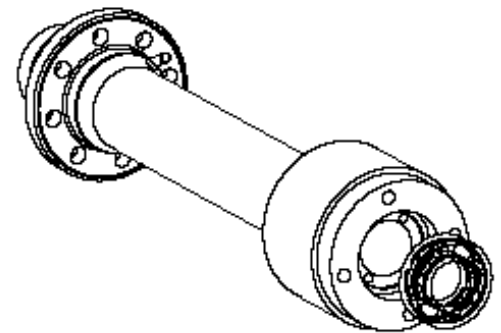
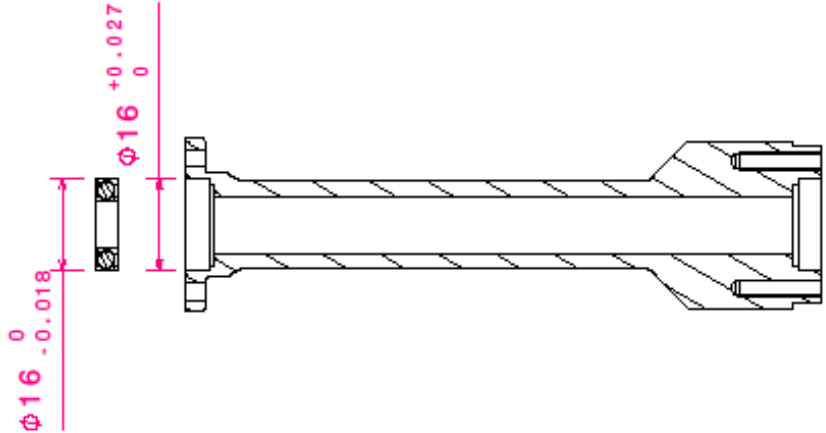
ISO Hole Tolerances

Example: Nominal Size 3mm-6mm; $28\mu\text{m} = 28 \times (10^{-3}) = 0.028\text{mm}$

Grade	NOMINAL HOLE SIZES (mm)																			
over	3	6	10	18	30	40	50	65	80	100	120	140	160	180	200	225	250	280	315	355
inc.	6	10	18	30	40	50	65	80	100	120	140	160	180	200	225	250	280	315	355	400
E6	+28 +20	+34 +25	+43 +32	+53 +40	+66 +50	+79 +60	+94 +72	+110 +85	+129 +100	+142 +110	+161 +125									
E7	+32 +20	+40 +25	+50 +32	+61 +40	+75 +50	+90 +60	+107 +72	+125 +85	+146 +100	+162 +110	+185 +125									
E11	+95 +20	+115 +25	+142 +32	+170 +40	+210 +50	+250 +60	+292 +72	+335 +85	+390 +100	+430 +110	+485 +125									
E12	+140 +20	+175 +25	+212 +32	+250 +40	+300 +50	+360 +60	+422 +72	+485 +85	+560 +100	+630 +110	+695 +125									
E13	+200 +20	+245 +25	+302 +32	+370 +40	+440 +50	+520 +60	+612 +72	+715 +85	+820 +100	+920 +110	+1 015 +125									
F6	+18 +10	+22 +13	+27 +16	+33 +20	+41 +25	+49 +30	+58 +36	+68 43	+79 +50	+88 +56	+98 +62									
F7	+22 +10	+28 +13	+34 +16	+41 +20	+50 +25	+60 +30	+71 +36	+83 43	+96 +50	+108 +56	+119 +62									
F8	+28 +10	+35 +13	+43 +16	+53 +20	+64 +25	+76 +30	+90 +36	+106 43	+122 +50	+137 +56	+151 +62									
G6	+12 +4	+14 +5	+17 +6	+20 +7	+25 +9	+29 +10	+34 +12	+39 +14	+44 +15	+49 +17	+54 +18									
G7	+16 +4	+20 +5	+24 +6	+28 +7	+34 +9	+40 +10	+47 +12	+54 +14	+61 +15	+69 +17	+75 +18									
G8	+22 +4	+27 +5	+33 +6	+40 +7	+48 +9	+56 +10	+66 +12	+77 +14	+87 +15	+98 +17	+107 +18									
H6	+8 0	+9 0	+11 0	+13 0	+16 0	+19 0	+22 0	+25 0	+29 0	+32 0	+36 0									
H7	+12 0	+15 0	+18 0	+21 0	+25 0	+30 0	+35 0	+40 0	+46 0	+52 0	+57 0									
H8	+18 0	+22 0	+27 0	+33 0	+39 0	+46 0	+54 0	+63 0	+72 0	+81 0	+89 0									
H9	+30 0	+36 0	+43 0	+52 0	+62 0	+74 0	+87 0	+100 0	+115 0	+130 0	+140 0									
H10	+48 0	+58 0	+70 0	+84 0	+100 0	+120 0	+140 0	+160 0	+185 0	+210 0	+230 0									
H11	+75 0	+90 0	+110 0	+130 0	+160 0	+190 0	+220 0	+250 0	+290 0	+320 0	+360 0									

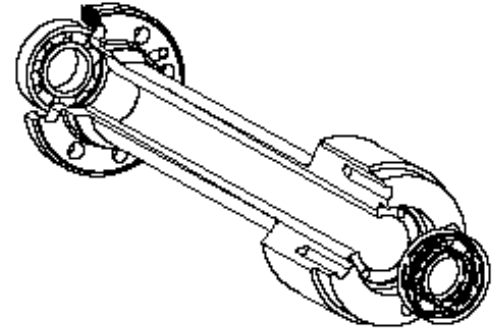
Static rod and bearing fitting

3.2 ✓



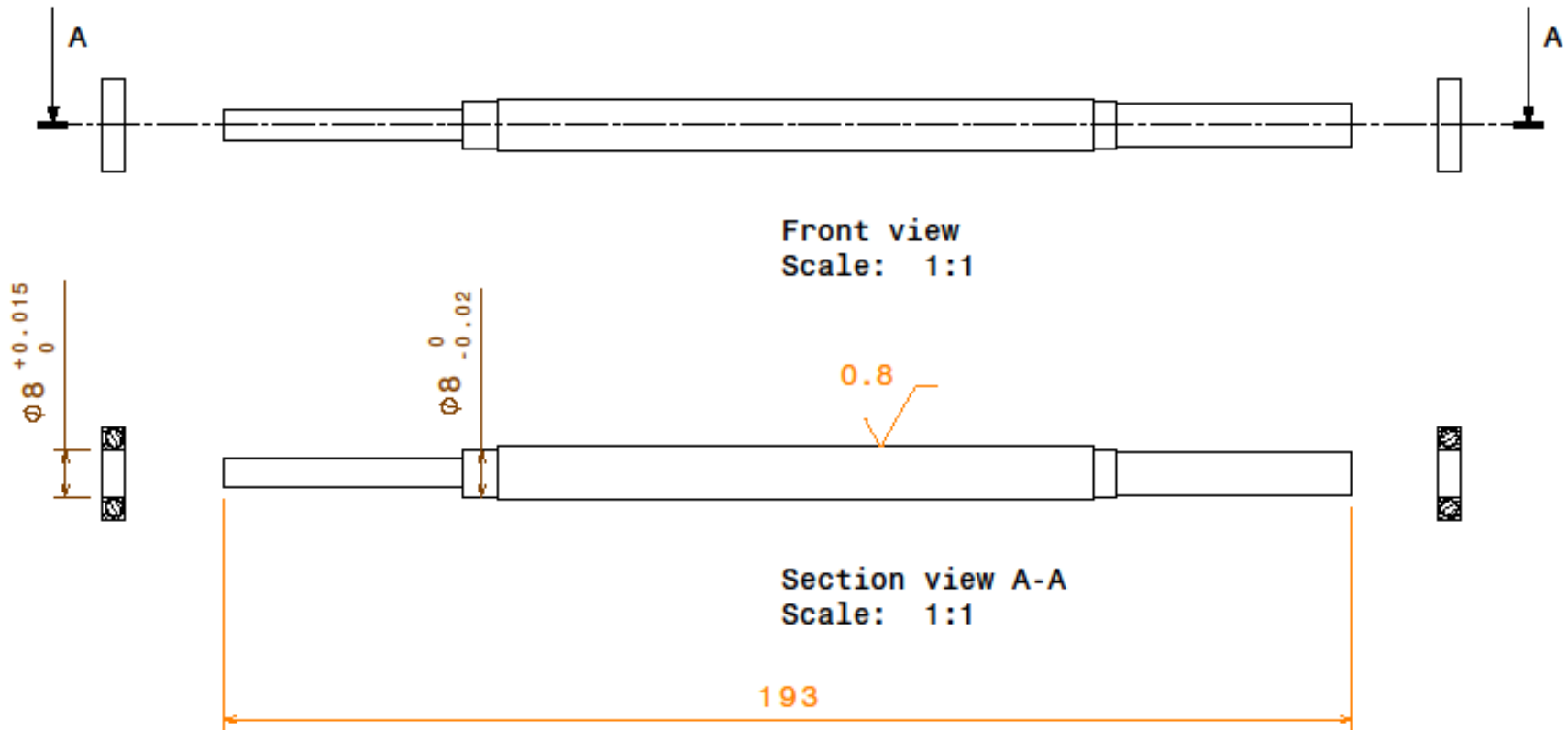
Isometric view
Scale: 1:1

Section view A-A
Scale: 1:1

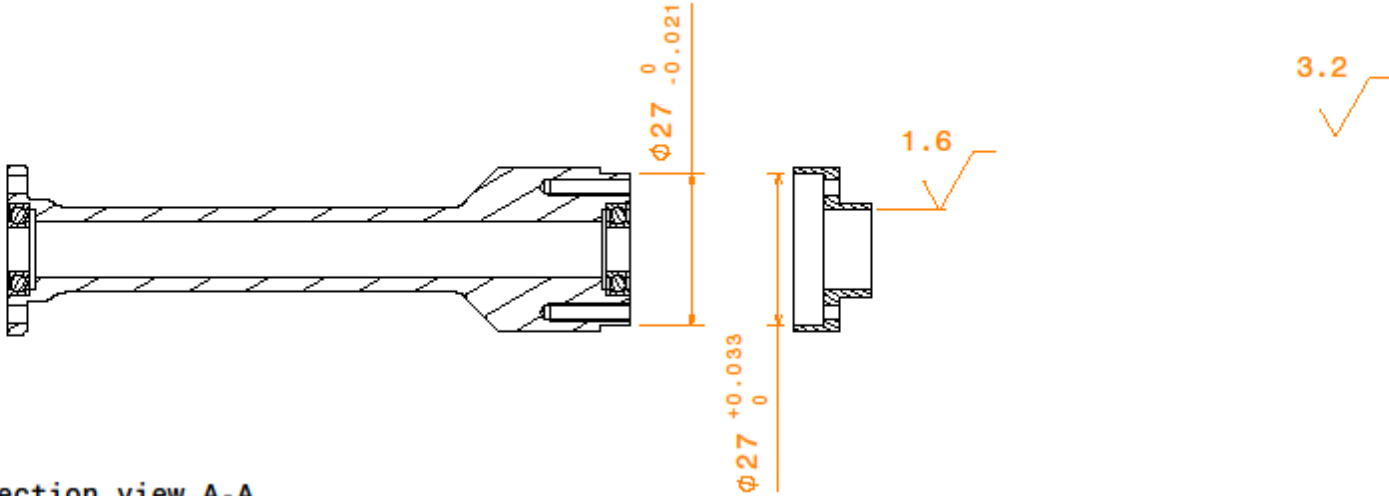


Isometric view
Scale: 1:1

Shaft and Bearing fitting



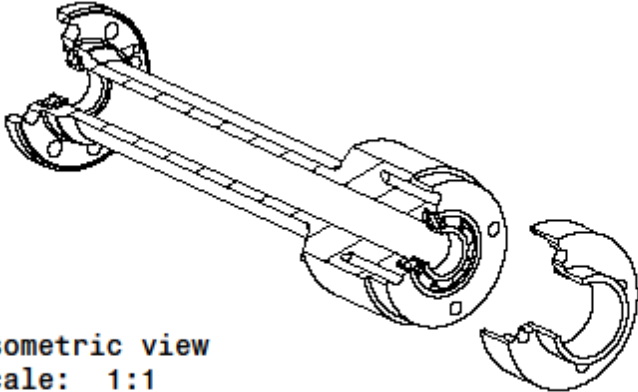
Static rod and Oil seal fitting



Section view A-A
Scale: 1:1

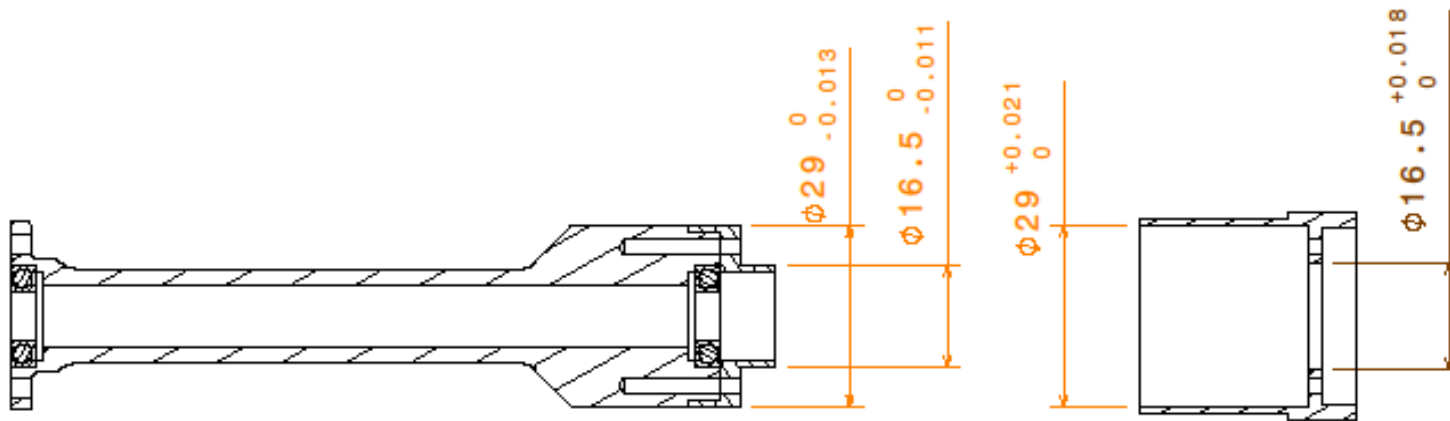


Front view
Scale: 1:1

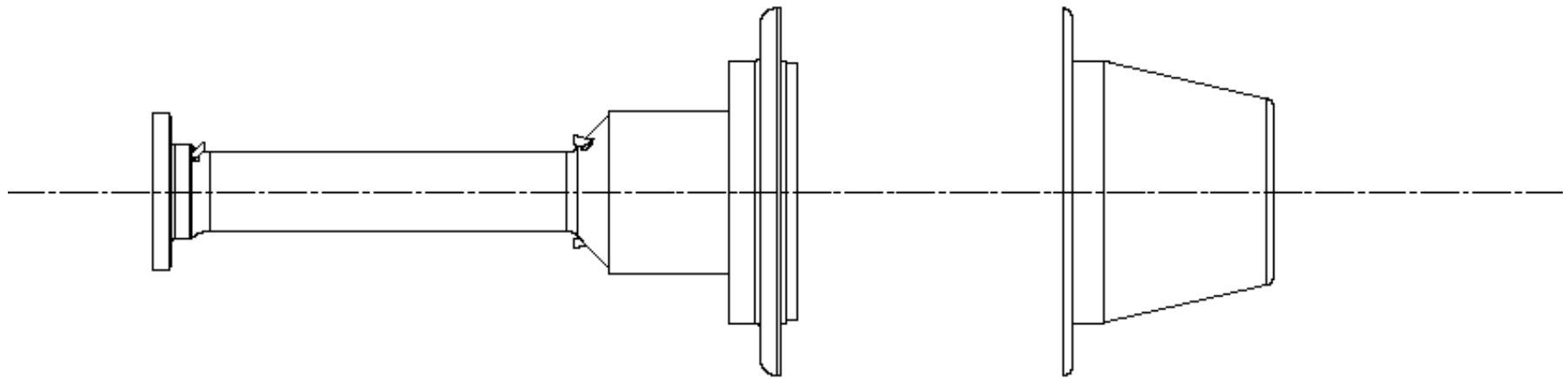


Isometric view
Scale: 1:1

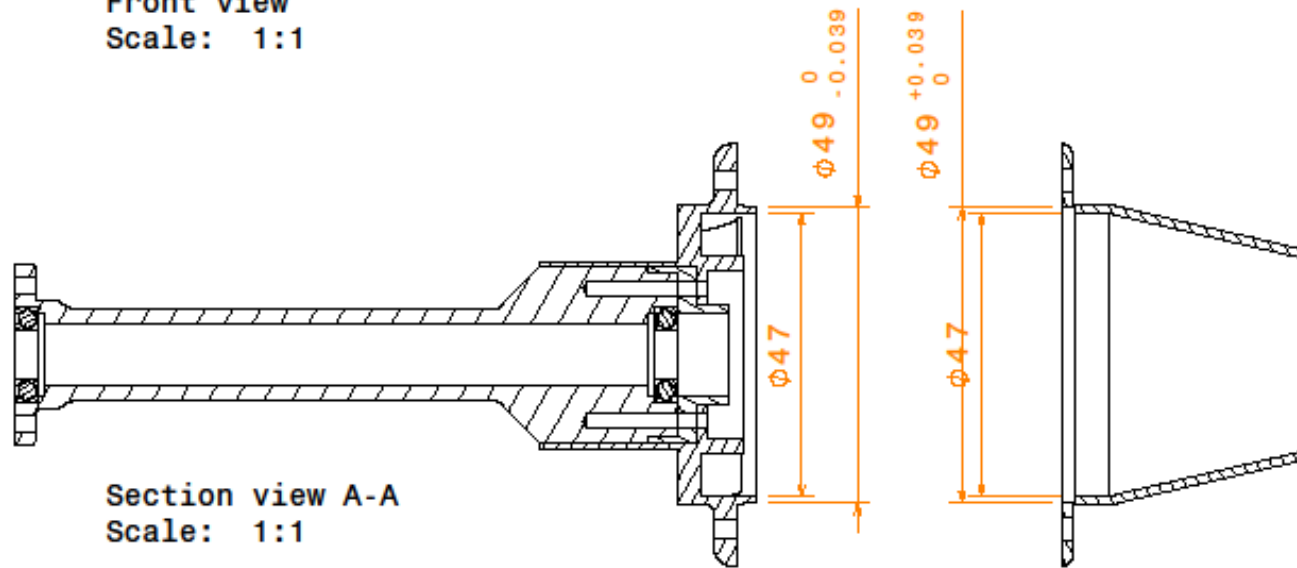
turbine stator fitting



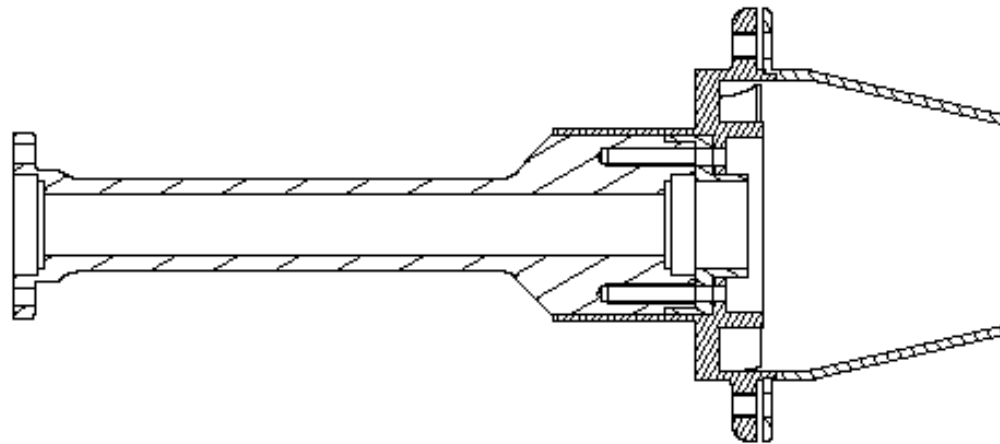
Section view A-A
Scale: 1:1



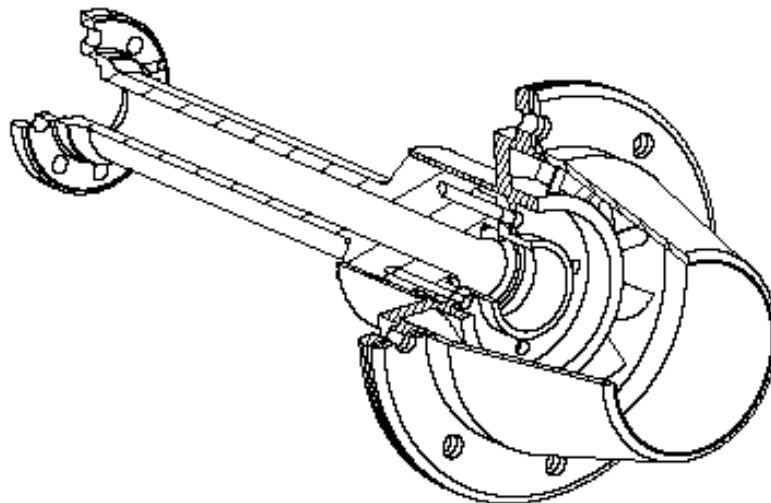
Front view
Scale: 1:1



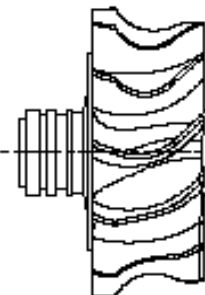
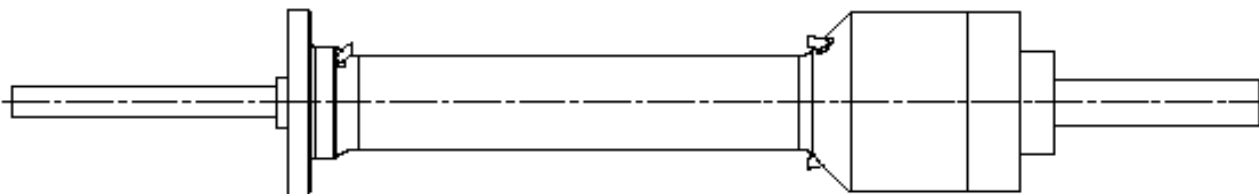
Section view A-A
Scale: 1:1



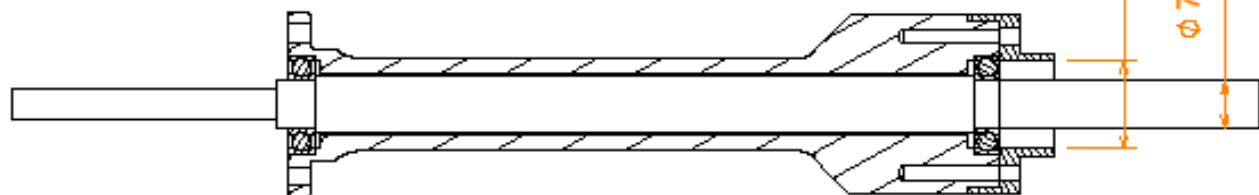
Section view A-A
Scale: 1:1



Isometric view
Scale: 1:1



Front view
Scale: 1:1

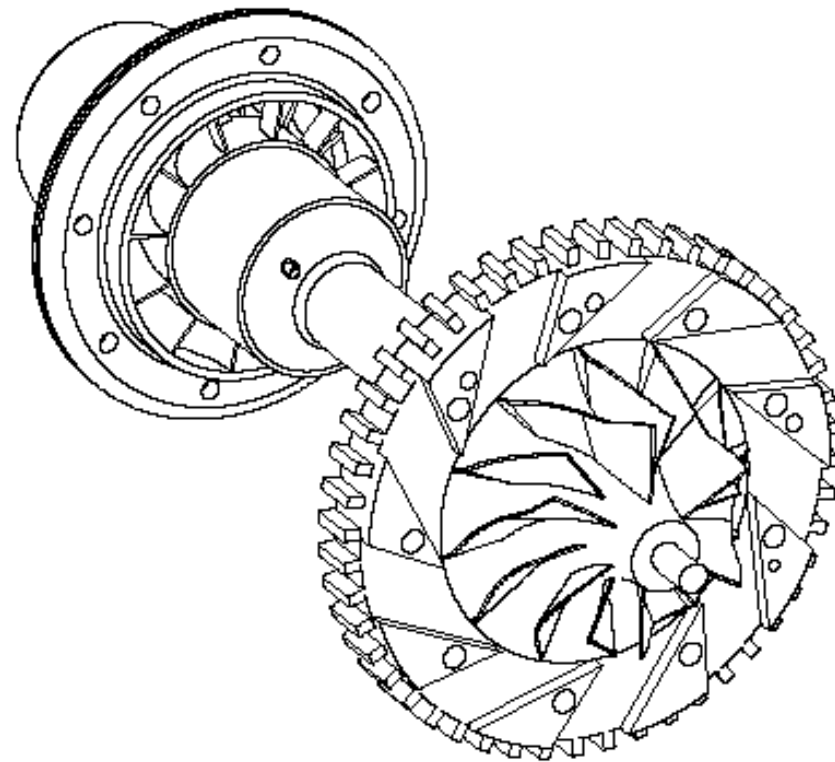


$\phi 14 \begin{smallmatrix} 0 \\ -0.03 \end{smallmatrix}$
 $\phi 7.55 \begin{smallmatrix} +0.013 \\ 0 \end{smallmatrix}$

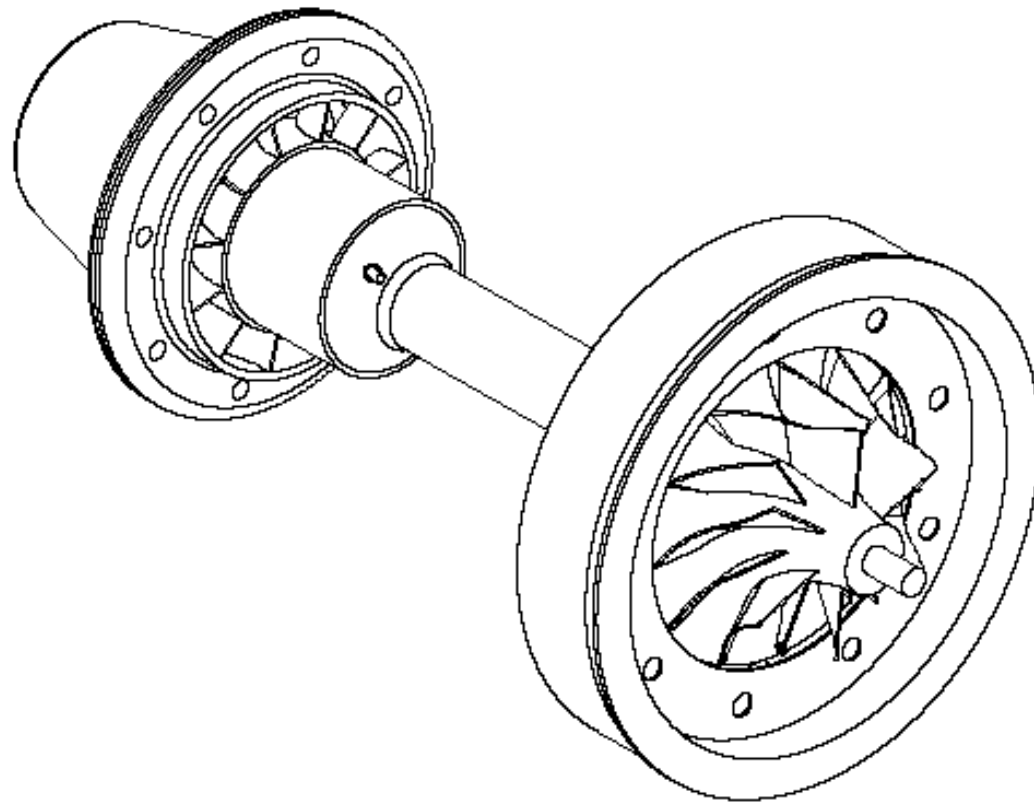
$\phi 13.9$

$\phi 7.55 \begin{smallmatrix} 0 \\ -0.022 \end{smallmatrix}$

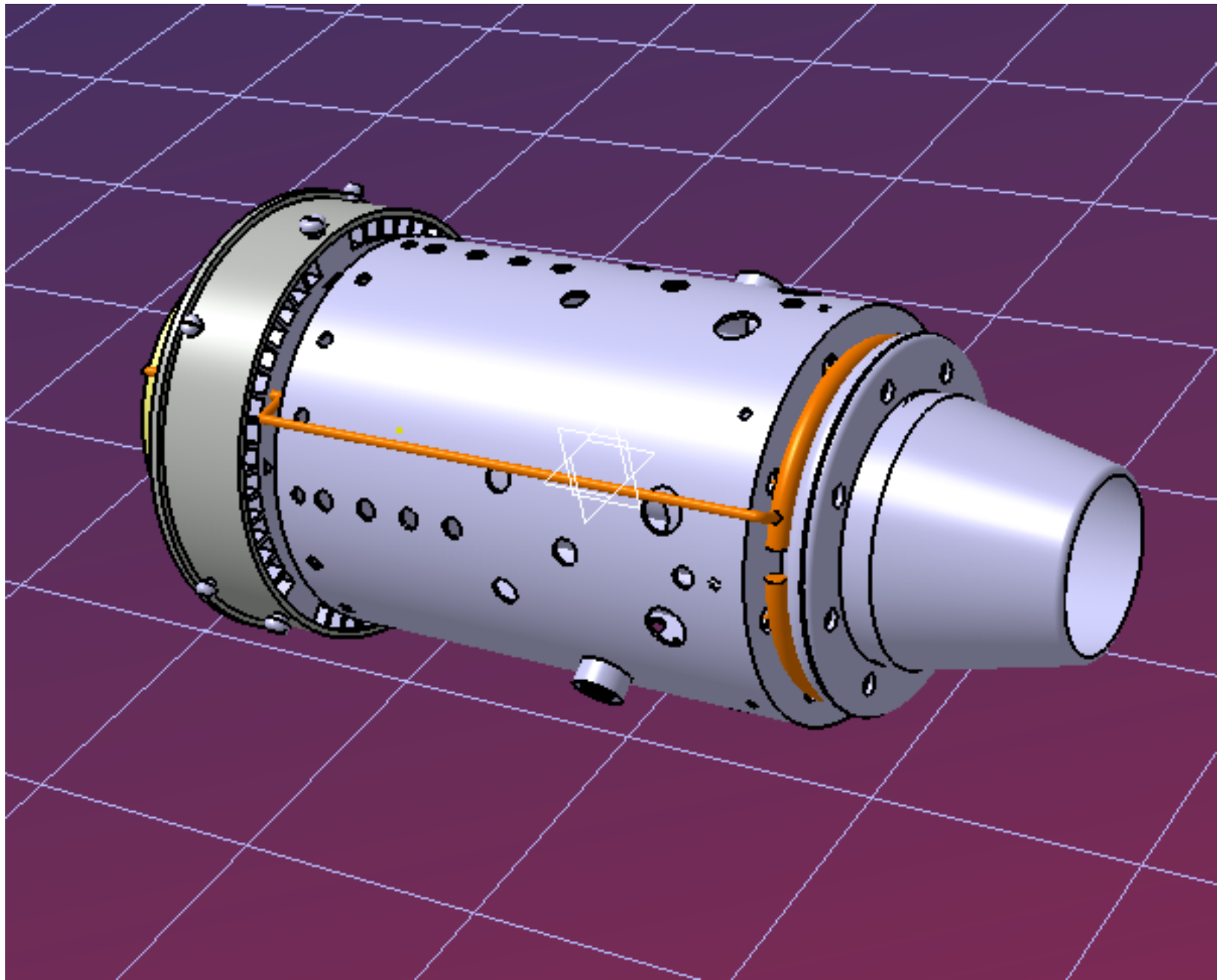
Section view A-A
Scale: 1:1

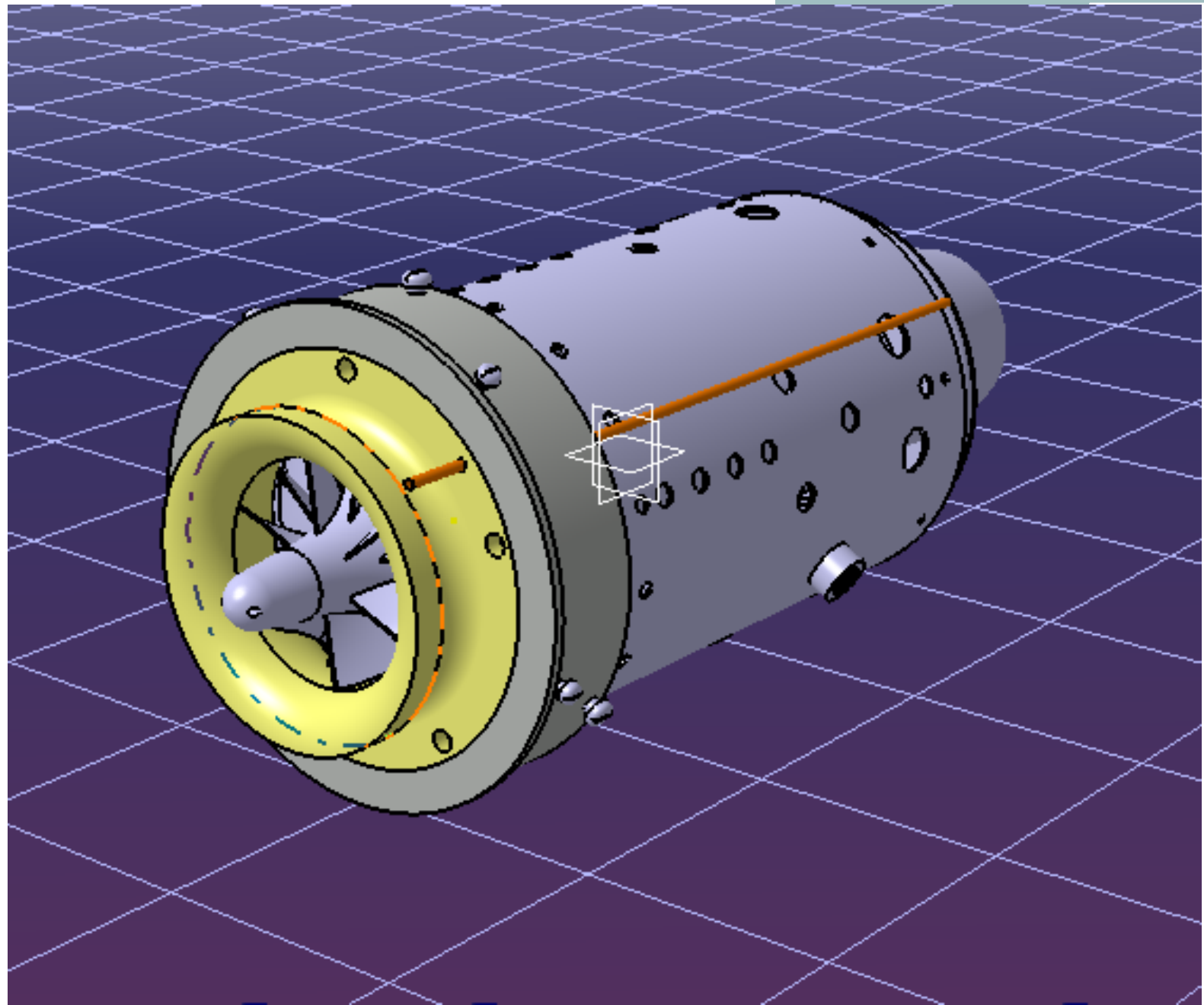


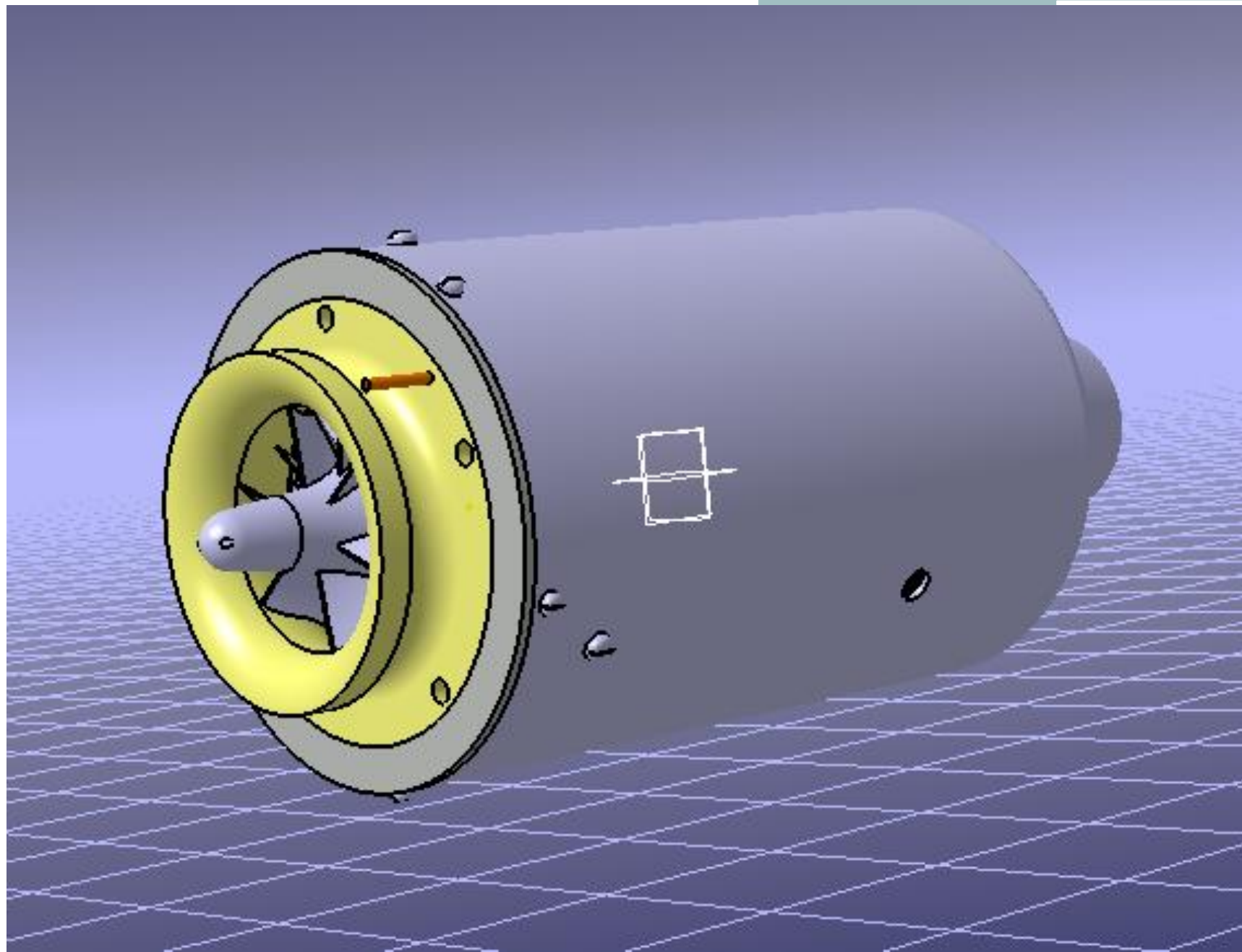
Isometric view
Scale: 1:1



Isometric view
Scale: 1:1





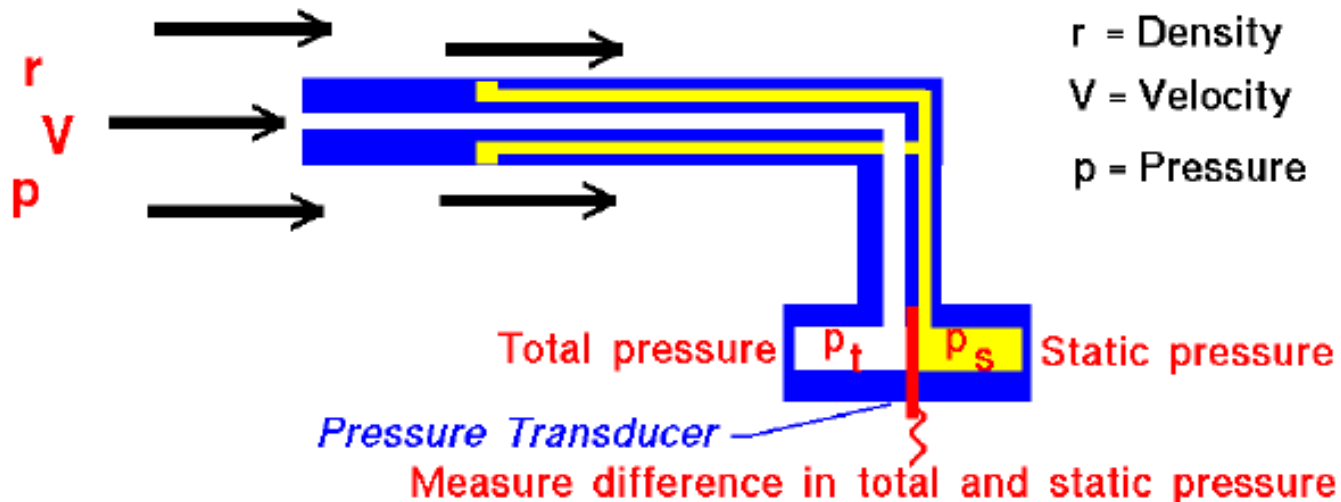


Mass Flow Rate



Pitot Tube

Glenn
Research
Center



Bernoulli's Equation :

static pressure + dynamic pressure = total pressure

$$(p_s + r \times \frac{V^2}{2}) = p_t$$

Solve for Velocity :

$$V^2 = \frac{2(p_t - p_s)}{r}$$



Mass Flow Rate

- $\dot{M} = \rho \cdot V \cdot S$
- ρ is density
- V is velocity
- S is section area

- Another way to calculate MFR



Stoichiometric Ratio

- Kerosene: $C_{12}H_{26}$ alkane or cycloalkane
- Kerosene: C_xH_y x ranges from 6 to 16
- Alkanes C_nH_{2n+2}
- $C_xH_y + (x+(y/4))O_2 = xCO_2 + (y/2)H_2O$
- Balance: $2C_{12}H_{26} + 37O_2 = 24CO_2 + 26H_2O$
- Molar mass: Carbon(C) = 12.01
- Molar mass: Oxygen(O) = 16
- Molar mass: hydrogen(H) = 1.008
- Molecular weight of kerosene: 170.34 g/mol
- Molecular weight of oxygen: 32g/mol
- 3.47 kg of air to burn 1kg kerosene
- $3.47/0.23 = 15.11$ air/fuel ratio

Nozzle Flange Gap (example Saturn V)

C: Copy of Static Structural - Mechanical [ANSYS Multiphysics]

File Edit View Units Tools Help | Solve Show Errors Worksheet

Show Vertices Wireframe Show Mesh Random Colors Annotation Preferences

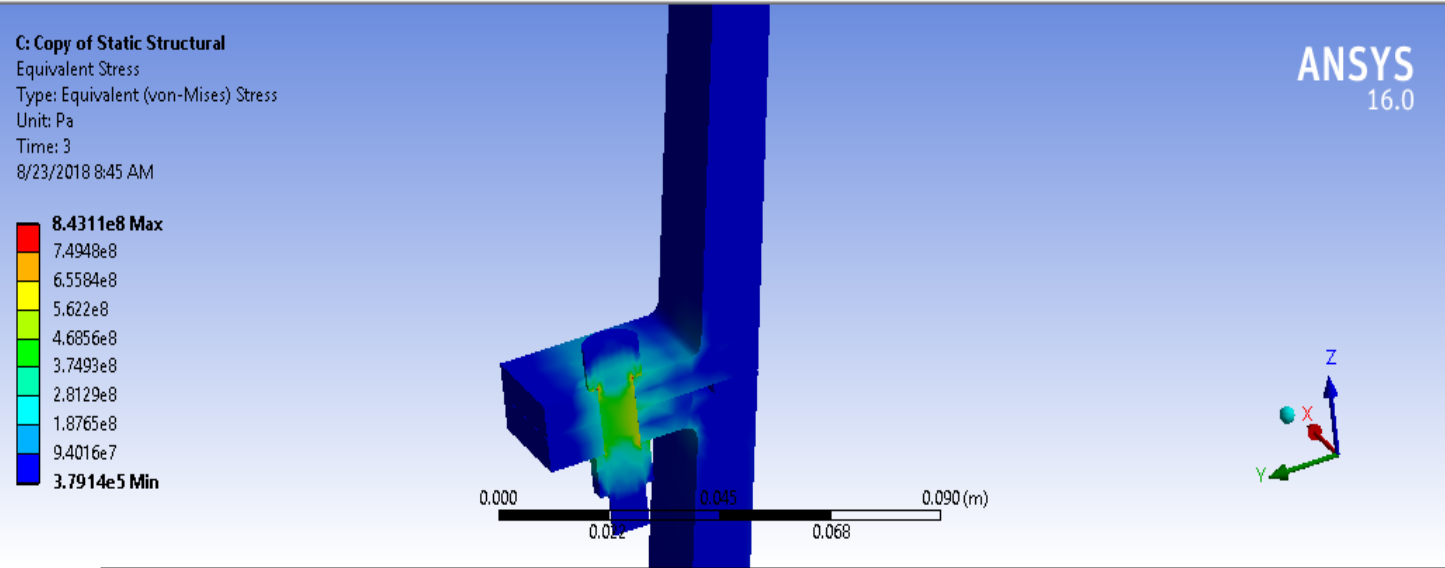
Explosive Factor: Assembly Center Edge Coloring Thicken Annotations

Result 1.0 (True Scale) Probe Display Scoped Bodies

Outline

Filter: Name

- Force_mid
- Bolt Pretension
- Solution (C6)**
 - Solution Information
 - Total Deformation t=1
 - Total Deformation t=2
 - Total Deformation t=3
 - Equivalent Stress
 - Normal Stress
 - Contact Tool
 - Status
 - Gap t=1
 - Gap t=2
 - Gap t=3
 - Bolt Pretension
 - Force Reaction



Details of "Equivalent Stress"

Scope

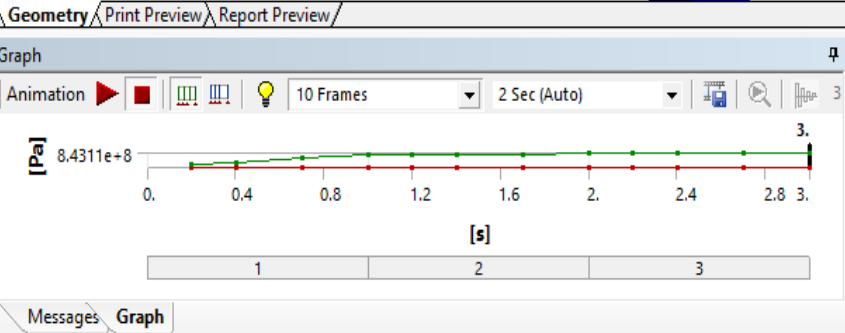
Scoping Method	Geometry Selection
Geometry	All Bodies

Definition

Type	Equivalent (von-Mises) Stress
By	Time
Display Time	Last
Calculate Time History	Yes
Identifier	
Suppressed	No

Integration Point Results

Display Option	Averaged
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Tabular Data

Time [s]	Minimum [Pa]	Maximum [Pa]
1 0.2	6.0242e-002	1.6829e+008
2 0.4	7.5238e-002	3.0879e+008
3 0.7	6.8654e-002	5.2017e+008
4 1.	5.6515e-002	7.3116e+008
5 1.2	2.4539e+005	7.3889e+008
6 1.4	3.0677e+005	7.5375e+008
7 1.7	3.5422e+005	7.8019e+008
8 2.	3.4827e+005	8.3337e+008
9 2.2	3.5422e+005	8.3337e+008

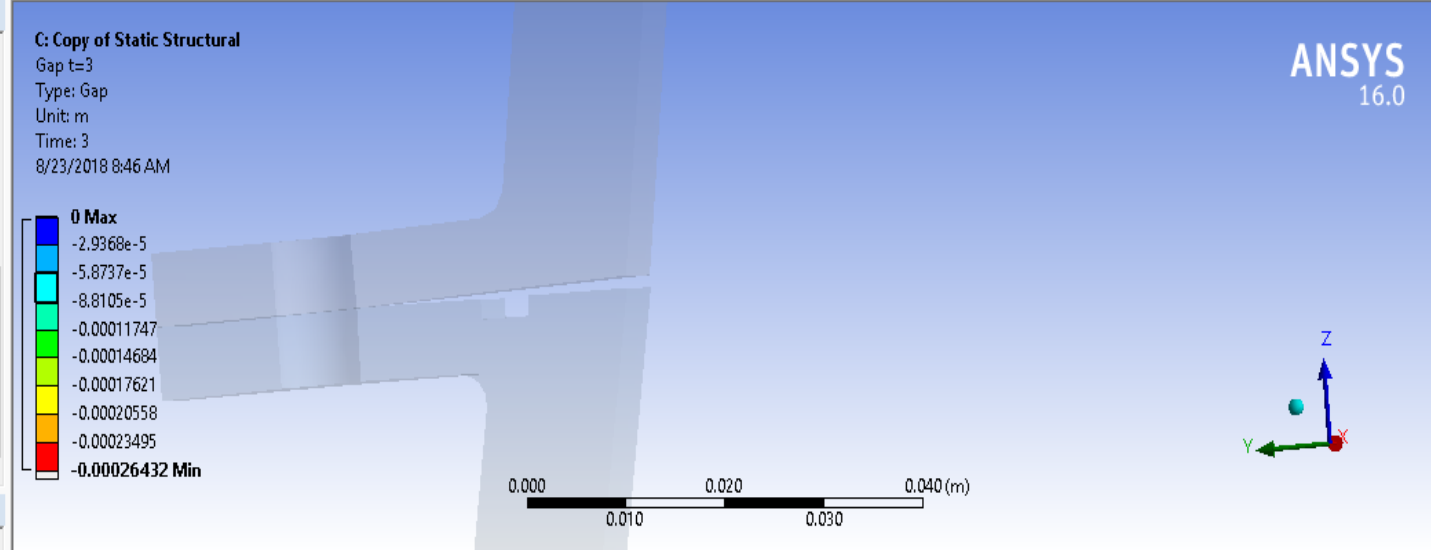
Outline

Filter: Name

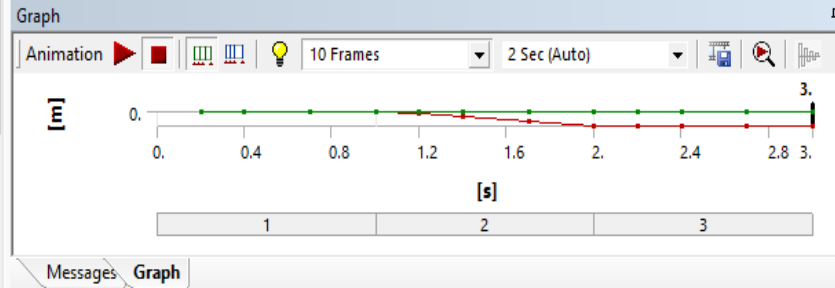
- Force_mid
- Bolt Pretension
- Solution (C6)**
 - Solution Information
 - Total Deformation t=1
 - Total Deformation t=2
 - Total Deformation t=3
 - Equivalent Stress
 - Normal Stress
 - Contact Tool
 - Status
 - Gap t=1
 - Gap t=2
 - Gap t=3
 - Bolt Pretension
 - Force Reaction

Details of "Gap t=3"

Definition	
Type	Gap
By	Time
<input type="checkbox"/> Display Time	3. s
Calculate Time History	Yes
Identifier	
Suppressed	No
Integration Point Results	
Display Option	Averaged
Results	
<input type="checkbox"/> Minimum	-2.6432e-004 m
<input type="checkbox"/> Maximum	0. m



Geometry Print Preview Report Preview



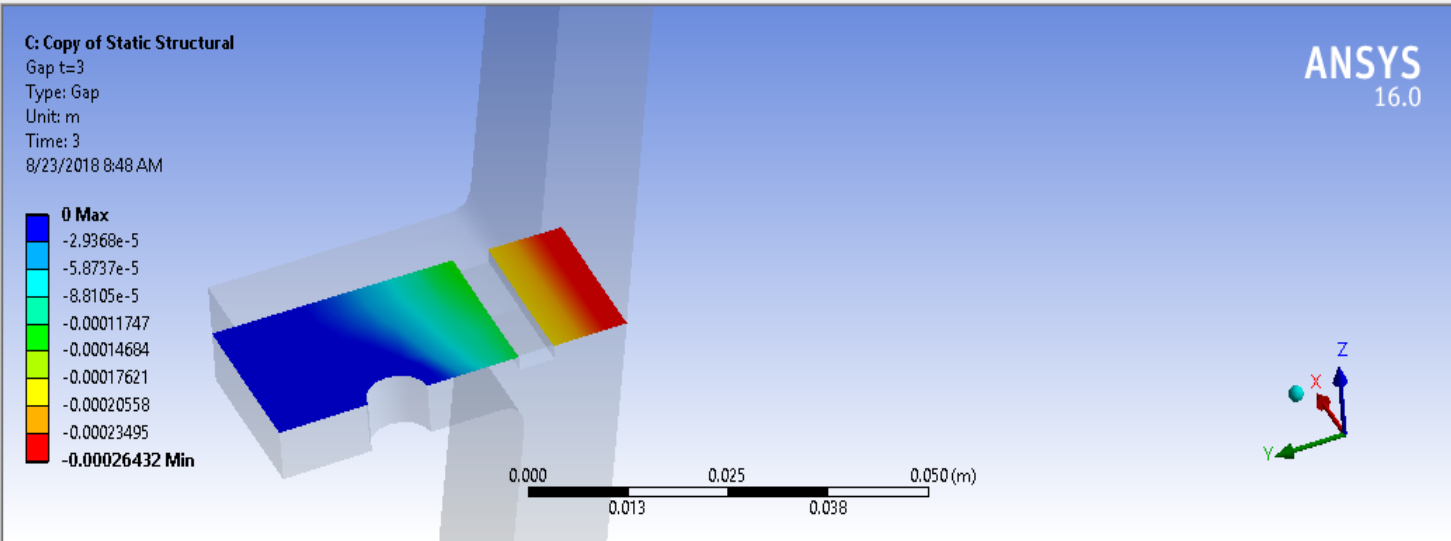
Tabular Data

Time [s]	Minimum [m]	Maximum [m]
1 0.2	-1.7511e-006	0.
2 0.4	-3.4746e-006	0.
3 0.7	-6.1683e-006	0.
4 1.	-8.9576e-006	0.
5 1.2	-4.3889e-005	0.
6 1.4	-9.1685e-005	0.
7 1.7	-1.749e-004	0.
8 2.	-2.6547e-004	0.
9 2.2	-2.6525e-004	0.

Outline

Filter: Name

- Force_mid
- Bolt Pretension
- Solution (C6)**
 - Solution Information
 - Total Deformation t=1
 - Total Deformation t=2
 - Total Deformation t=3
 - Equivalent Stress
 - Normal Stress
 - Contact Tool
 - Status
 - Gap t=1
 - Gap t=2
 - Gap t=3
 - Bolt Pretension
 - Force Reaction



Details of "Gap t=3"

Definition

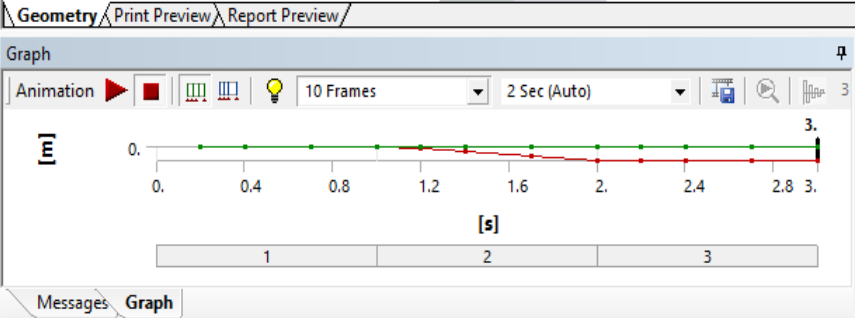
Type	Gap
By	Time
Display Time	3. s
Calculate Time History	Yes
Identifier	
Suppressed	No

Integration Point Results

Display Option	Averaged
----------------	----------

Results

Minimum	-2.6432e-004 m
Maximum	0. m



Tabular Data

	Time [s]	Minimum [m]	Maximum [m]
1	0.2	-1.7511e-006	0.
2	0.4	-3.4746e-006	0.
3	0.7	-6.1683e-006	0.
4	1.	-8.9576e-006	0.
5	1.2	-4.3889e-005	0.
6	1.4	-9.1685e-005	0.
7	1.7	-1.749e-004	0.
8	2.	-2.6547e-004	0.
9	2.2	-2.6535e-004	0.

Future plans

- Finish manufacturing processes
- Make the engine start manually
- Working on ECU (electronic control unit)
- Estimate optimal working condition of the whole system



Thanks for listening